

NRC-CNRC

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Application de la norme CAN/CSA A123.24 pour évaluer la résistance au vent des toitures végétalisées

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CNRC - Construction

27 March, 2024



National Research
Council Canada

Conseil national de
recherches Canada

Canada



CSA
Group

A123.24-15

Standard test method for wind resistance
of modular vegetated roof assembly



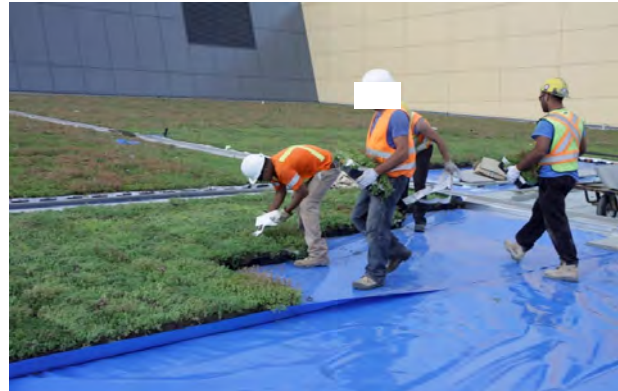
Équipe

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David Van Reenen**

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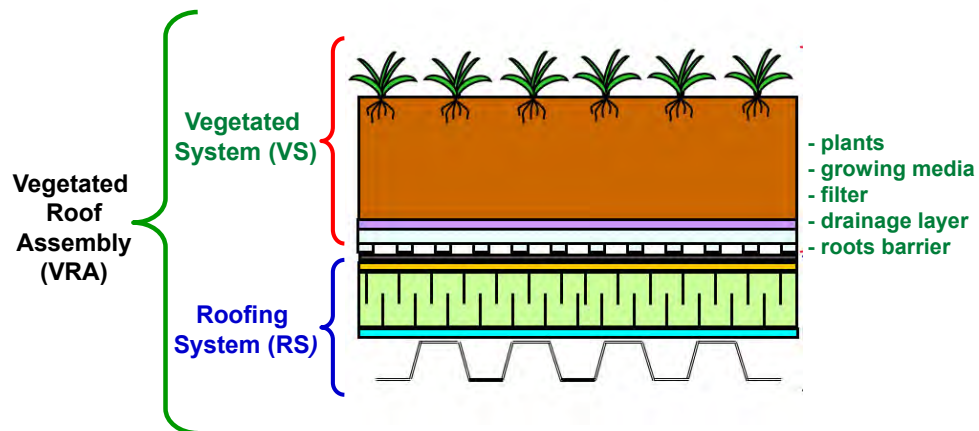
courtesy LiveRoof Ontario Inc.



courtesy LiveRoof Ontario Inc.

3

Vegetated Roof Assembly (VRA) Assemblage de toiture végétalisée



4

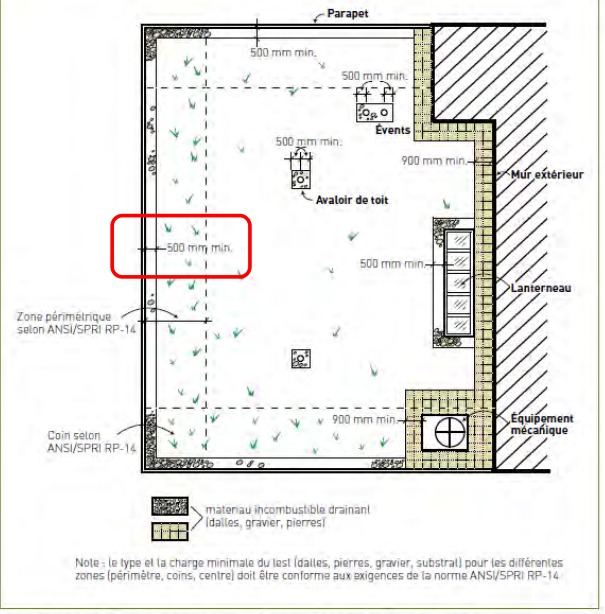


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4. Résistance au soulèvement dû au vent et à l'érosion

- 4.1. Le calcul des forces de soulèvement dû au vent doit être réalisé selon les exigences du Code.
- 4.2. Sous réserve des points 4.3 et 4.4, le toit végétalisé doit être conçu pour résister aux effets de soulèvement par le vent selon les critères de la norme ANSI/SPRI RP-14, «Wind Design Standard for Vegetative Roofing Systems», tout en respectant les recommandations du manufacturier de la membrane d'étanchéité.
- 4.3. La hauteur du parapet mesurée au-dessus du substrat ou du lest doit être calculée selon la norme ANSI/SPRI RP-14 et ne doit pas être inférieure à 150 mm.
- 4.4. Une zone libre de végétation d'une largeur d'au moins 500 mm et recouverte de lest de pierre ou de dalles de béton conforme aux règles de l'art et respectant la norme ANSI/SPRI RP-14 est requise entre le parapet et le couvert végétatif.
- 4.5. Des mesures de retenue conformes aux règles de l'art doivent être prises pour éviter l'érosion du substrat et pour contrer l'arrachement des plantes par le vent jusqu'à ce que le couvert végétatif ait atteint sa maturité.
- 4.6. Seules les membranes d'étanchéité à pleine adhérence ou les membranes fixées mécaniquement sont permises sur le bassin sur lequel le toit végétalisé est construit.



Zones libres de végétation et zones pour la résistance au soulèvement dû au vent

Note : le type et la charge minimale du lest (dalles, pierres, gravier, substrat) pour les différentes zones (périphérie, coins, centre) doit être conforme aux exigences de la norme ANSI/SPRI RP-14.

6

Guidelines providing specifications

7

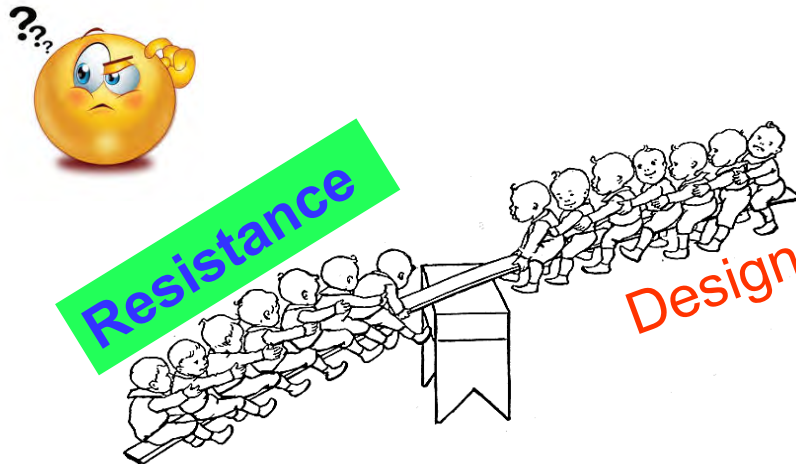
Guidelines providing specifications

Standard establishing pass/fail criteria

MISSING

8

Resistance vs Design of roof top add-ons

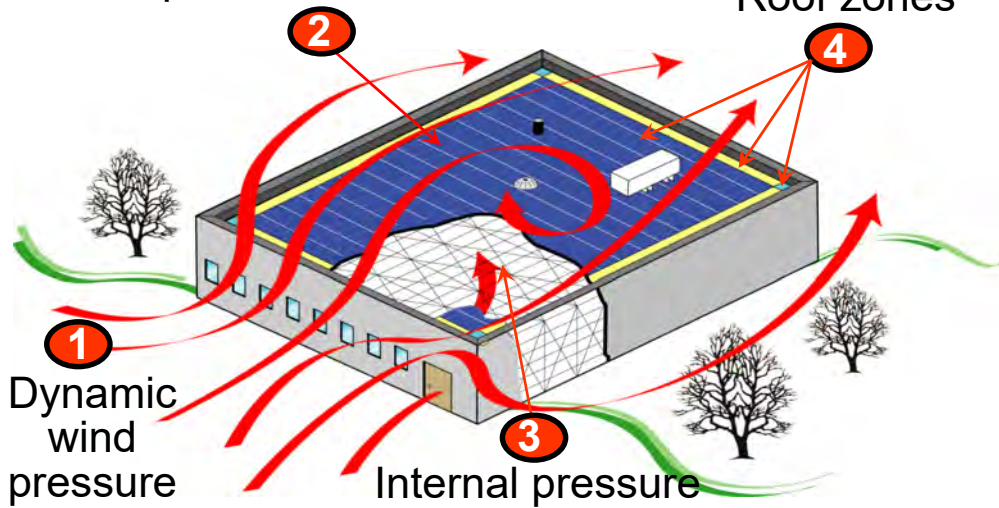


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Design of roof claddings

External pressure

Roof zones



10

Building Aerodynamics

Part 4 Structural Design

Table C-2 Climatic Design Data for Selected Locations in Canada

Pression dynamique, q (kPa)

Coeff pression, $C_p C_g$

4.1.7. Charge due au vent

$$p = I_W q C_e C_t C_g C_p \text{ (kPa)}$$

$$p_i = I_W q C_{ei} C_t C_{gi} C_{pi}$$

-2.8 kPa (corner)

-1.4 kPa (edge)

-1.1 kPa (interior)

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Wind uplift resistance

5.2.2.2. Charges dues au vent (Voir la note A-5.2.2.2.)

1) Le présent article s'applique à la détermination de la charge due au vent prise en compte dans le calcul des matériaux, composants ou ensembles de construction, y compris leurs assemblages, séparant des milieux différents ou exposés au milieu extérieur, si ces éléments :

- sont soumis à une charge due au vent; et
- doivent être conçus de façon à résister à une charge due au vent.

2) Sous réserve du paragraphe 3), la charge due au vent décrite au paragraphe 1) doit représenter la totalité de la charge spécifiée due au vent calculée selon l'article 4.1.7.1.

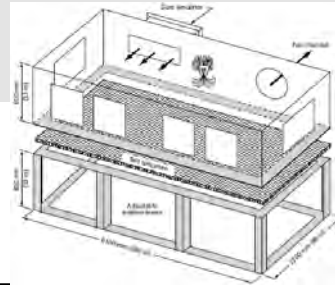
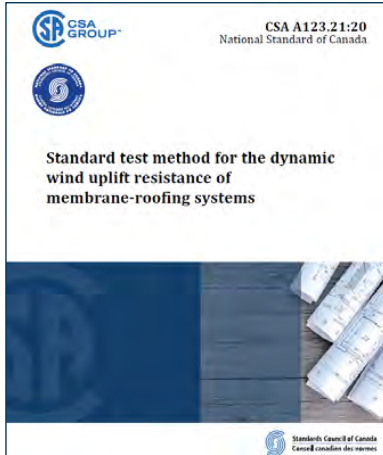
3) Si l'on peut démontrer au moyen d'essais ou d'analyses qu'un matériau, composant ou ensemble de construction ou assemblage décrit au paragraphe 1) est exposé à des charges dues au vent inférieures à la totalité des charges dues au vent spécifiées, la charge décrite au paragraphe 1) ne doit pas être inférieure à la valeur établie au moyen d'un essai ou d'une analyse.

4) Sous réserve du paragraphe 5), la résistance à l'arrachement sous l'action du vent des couvertures à membrane doit être déterminée conformément à la norme CAN/CSA-A123.21, « Méthode d'essai normalisée de la résistance dynamique à l'arrachement sous l'action du vent des systèmes de couverture à membrane » (voir la note A-5.2.2.2. 4)).

5) Les couvertures à membrane ayant une performance déjà éprouvée pour les charges dues au vent prévues ne sont pas visées par le paragraphe 4) (voir la note A-5.1.4.1. 5)).

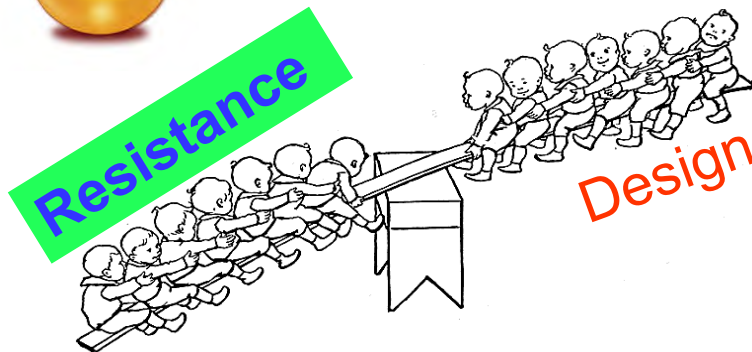


Wind uplift resistance



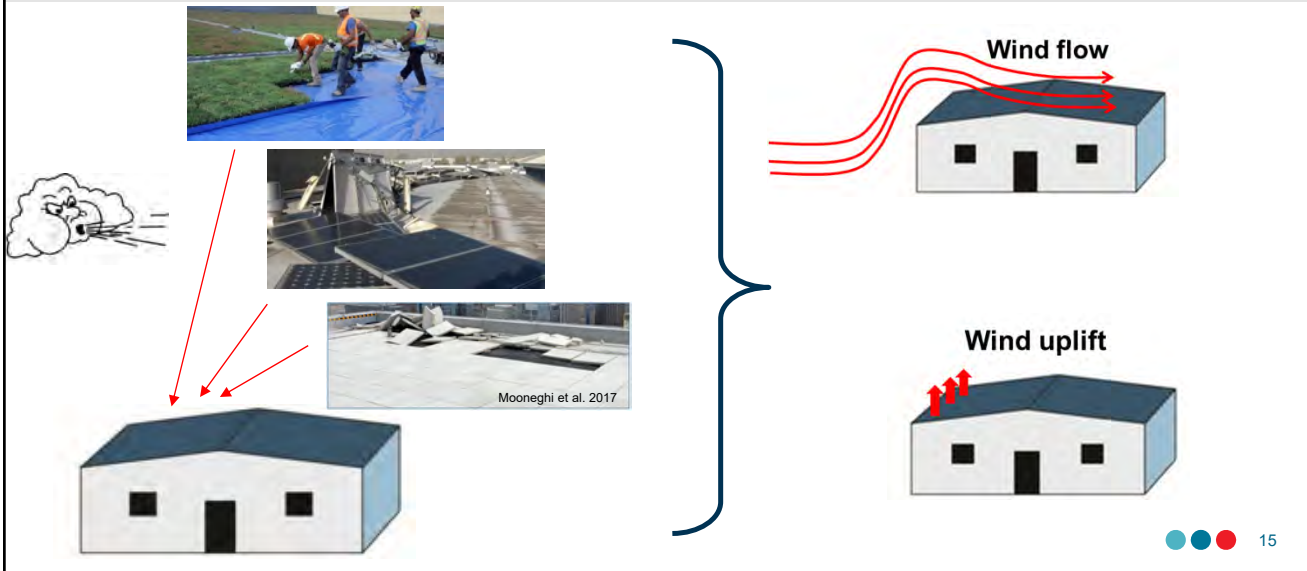
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Resistance vs Design of VRA

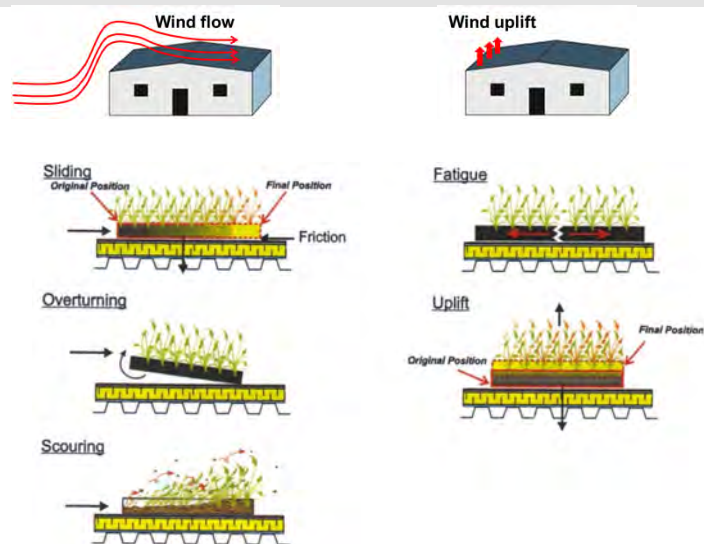


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Wind resistance of roof top add-ons



Wind Resistance of Roof top add-ons



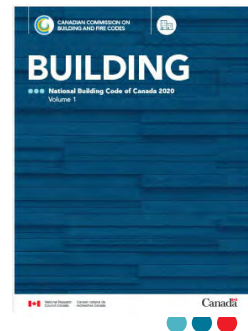
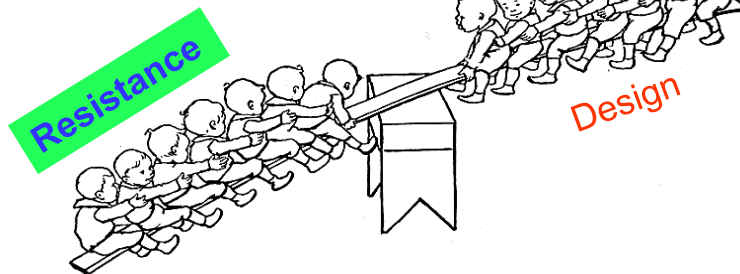
Evaluating VRA wind resistance



Wind Speed - mph



Pressure -psf



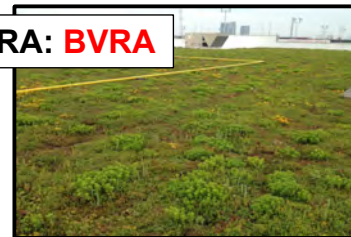
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VRA

Modular VRA: MVRA



Built-in-place VRA: BVRA



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A123.24-15

Standard test method for wind resistance
of modular vegetated roof assembly



2015 – MVRA only






CSA A123.24:21
National Standard of Canada



Standard test method for wind resistance
of vegetated roof assembly



2021 - MVRA AND BVRA




Standards Council of Canada
Conseil canadien des normes

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Flow Resistance

VRA Wind Resistance Test

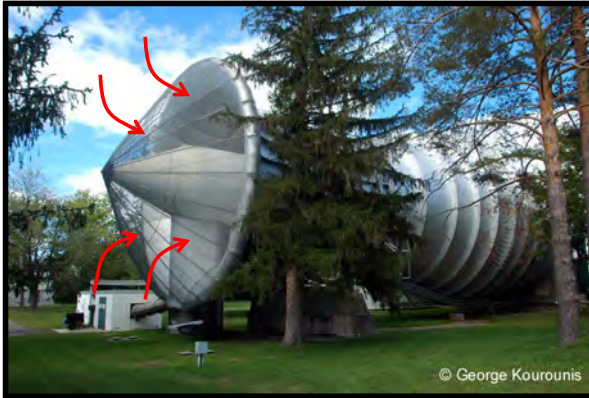
Wind Tunnel

Benchmarking - Data

Flow testing

Parametric study
Test procedure development

NRC wind tunnel

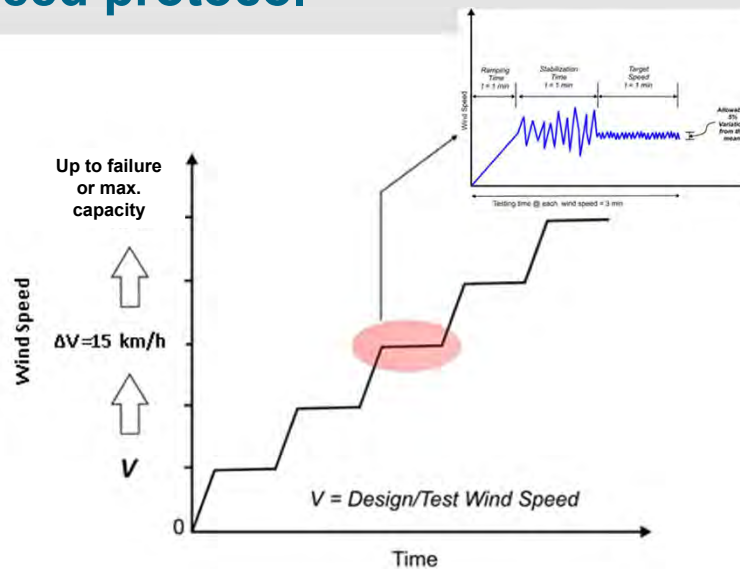


- 10' x 20'
- Open-circuit tunnel
- 100 mph wind



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Wind speed protocol



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MVRA



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MVRA – failure mode



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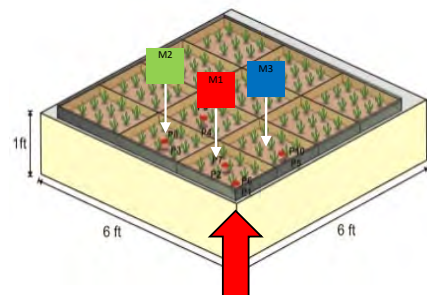
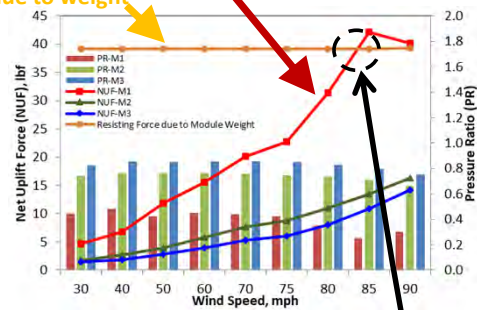
MVRA – failure mode



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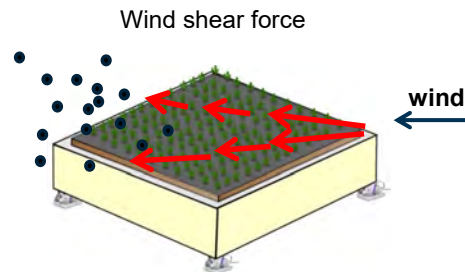
MVRA- failure mode

Net uplift force at the corner
Resisting force due to weight



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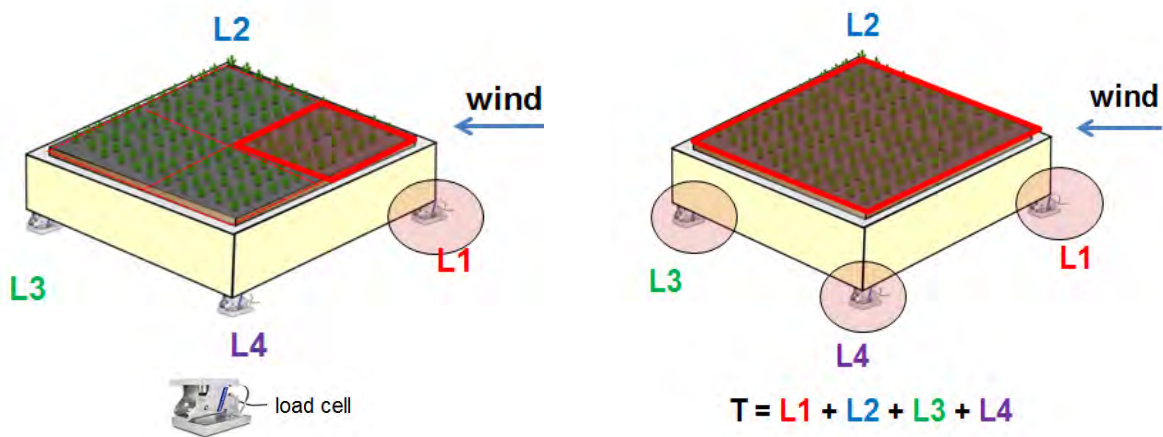
BVRA



- Intensity depends on wind speed
- **Growing media loss (erosion)**
- Continuous process

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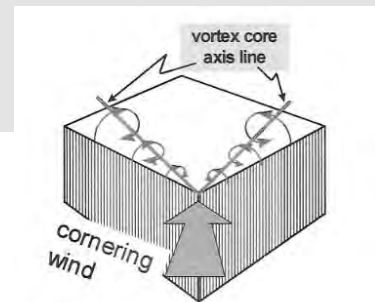
BVRA



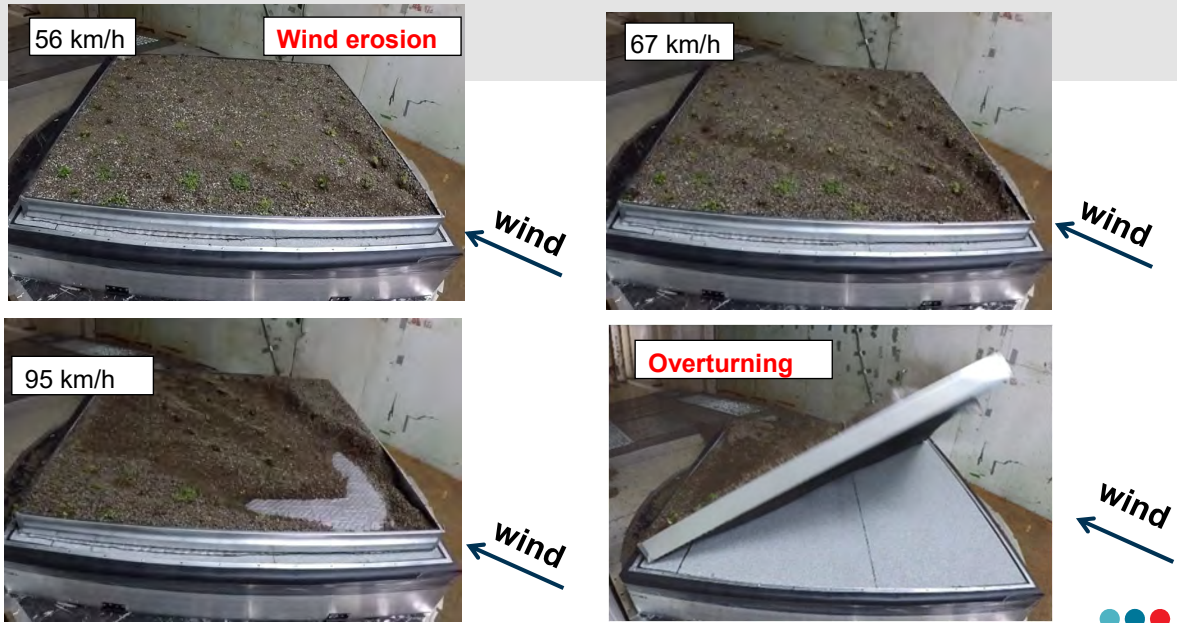
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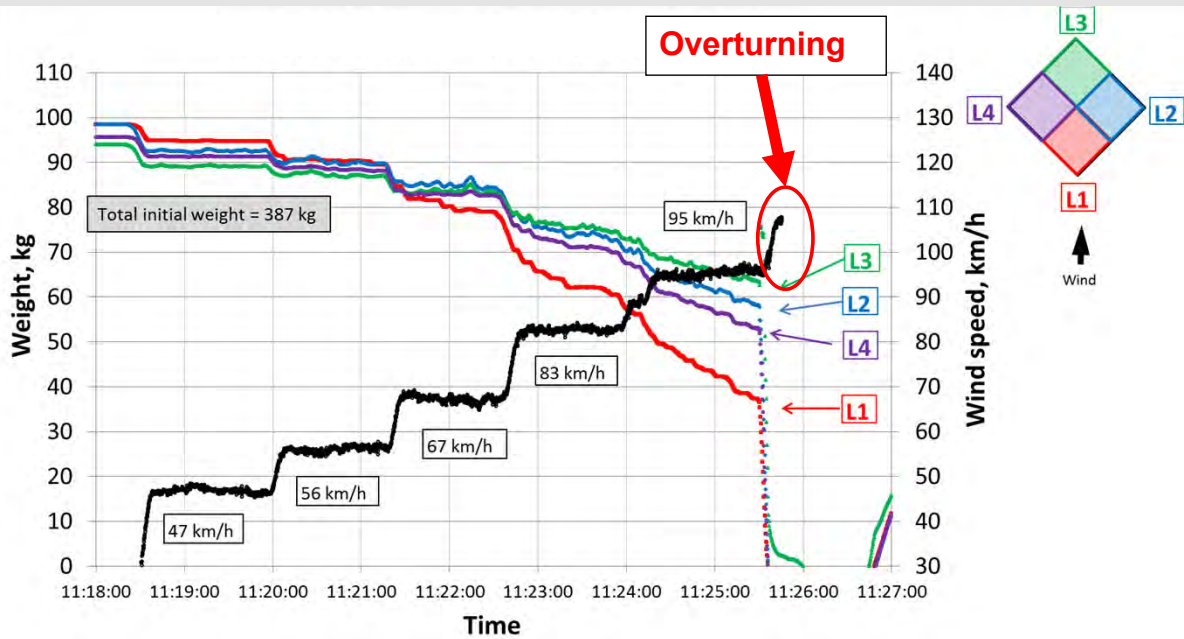
BVRA – failure mode



BVRA – failure mode

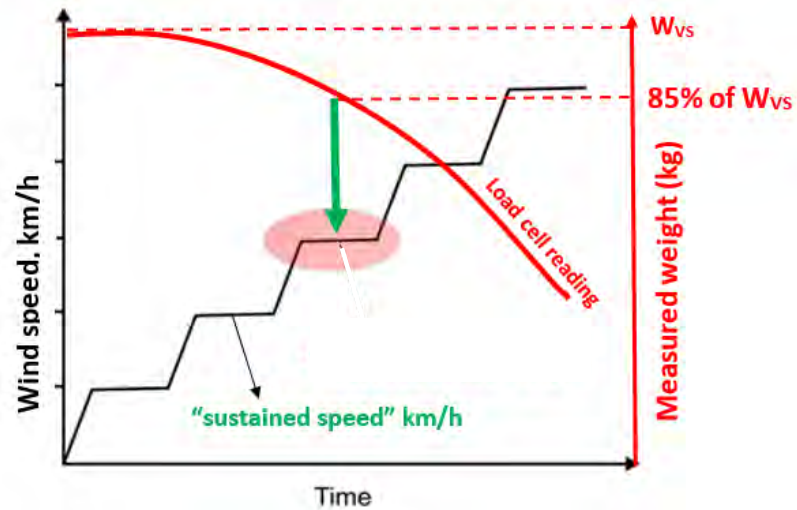


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Wind speed protocol + failure



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Flow Resistance

In a commercial lab

In collaboration with



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Wind flow facility

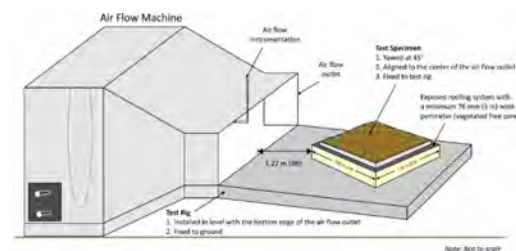
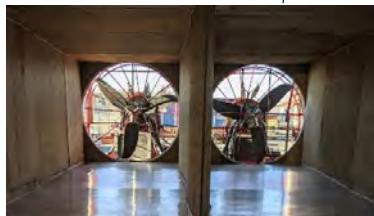
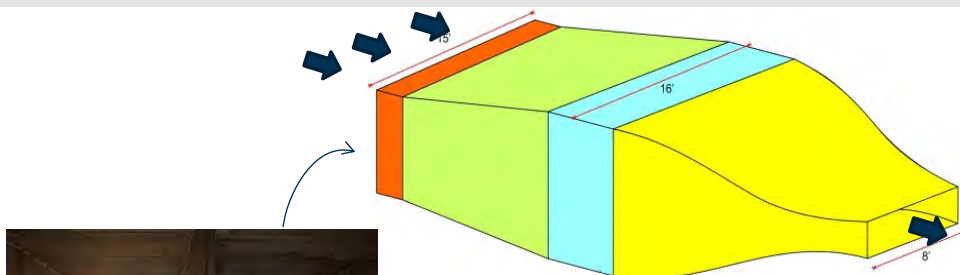


- 150 mph (240 km/h)



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Wind flow facility



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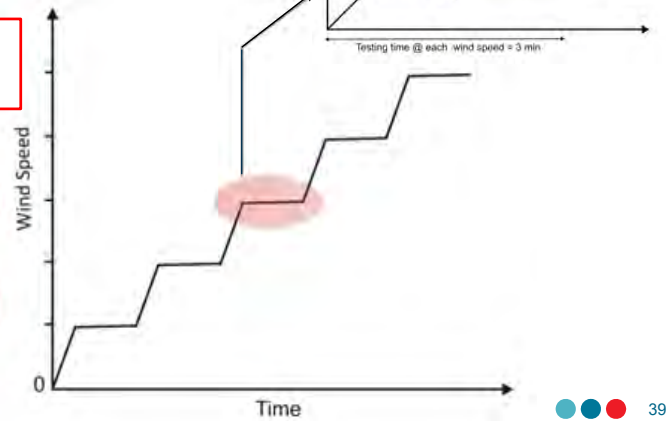
Wind speed protocol



Up to **failure**
or max. speed

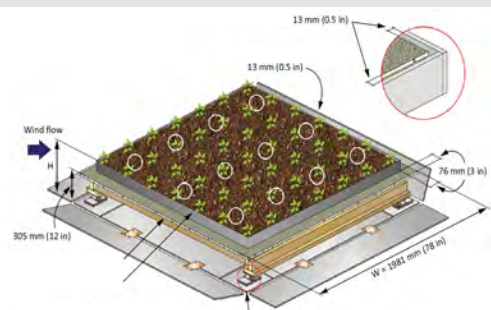
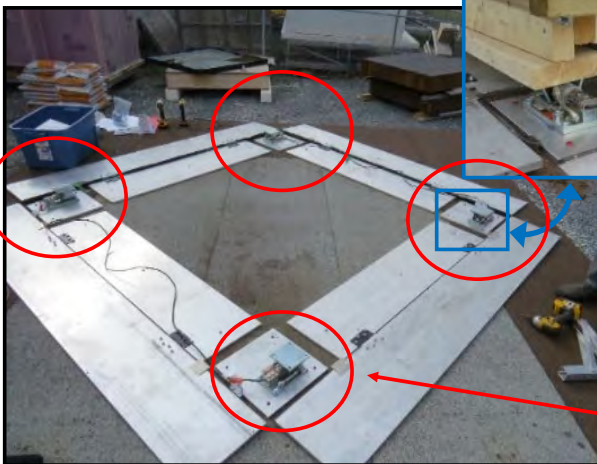
$\Delta V = 10 \text{ km/h}$

$V \text{ km/h}$



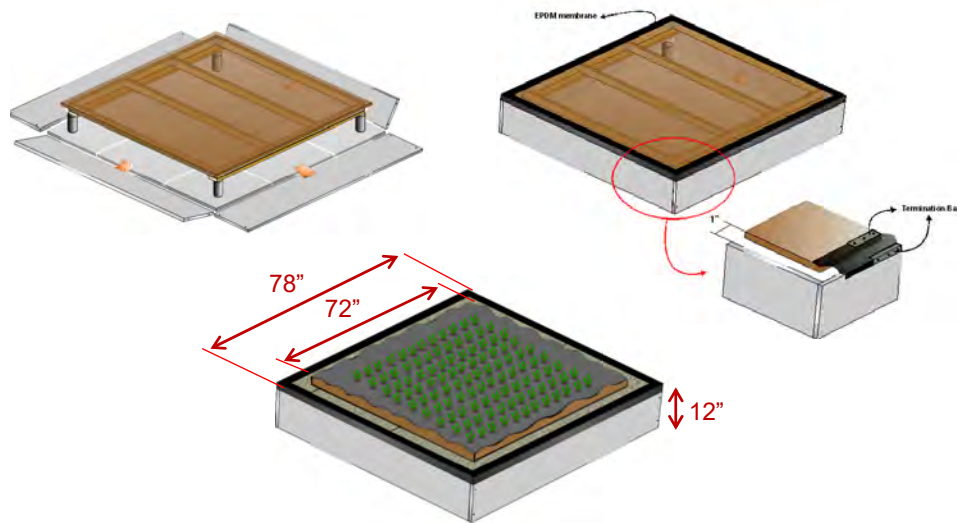
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Load cells



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BVRA construction



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BVRA installation



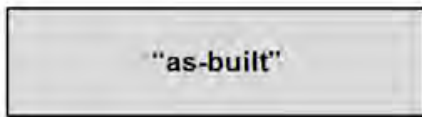
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BVRA challenges



Resistance ?

Effect of vegetation growth



Built-in-place :BVRA



- more than 40 specimens
- same plants (sedum)
- irrigation plan
- no fertilizer
- no replacement after a year

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Built-in-place VRA: BVRA

As-built



12-weeks



1-year



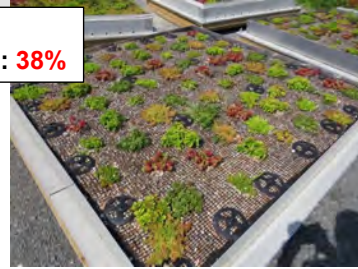
46

12-weeks

Source 1
Coverage: 68%



Source 2
Coverage: 38%



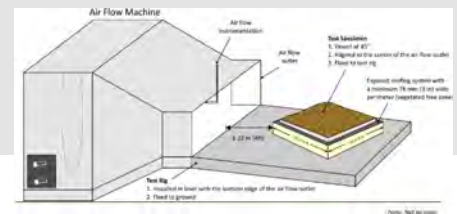
Source 3
Coverage: 78%



Source 4
Coverage: 90%



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Video 1 (source_1- as built)

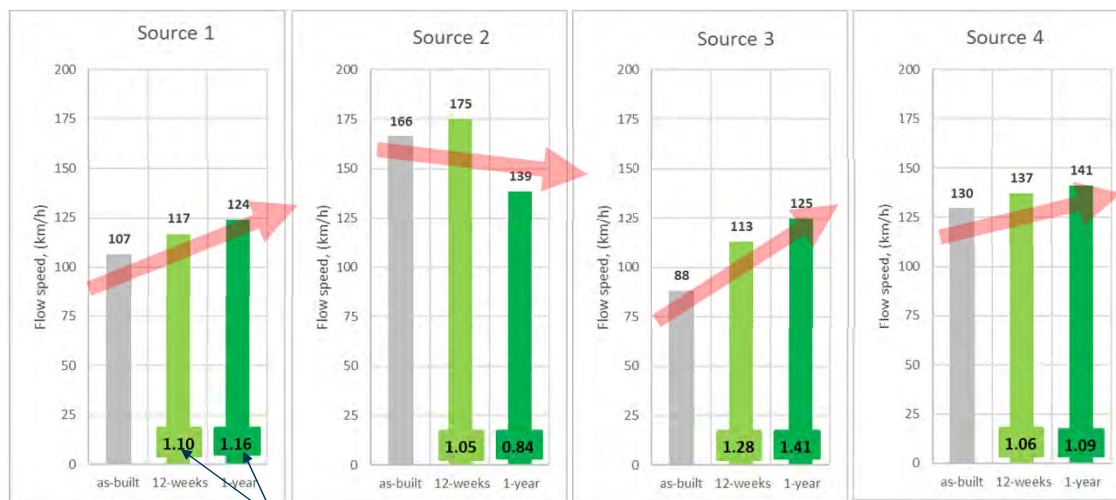
Video 2 (source_1- after 1 year)

Video 3 (source_2- as built)

Video 4 (source_2- after 1 year)

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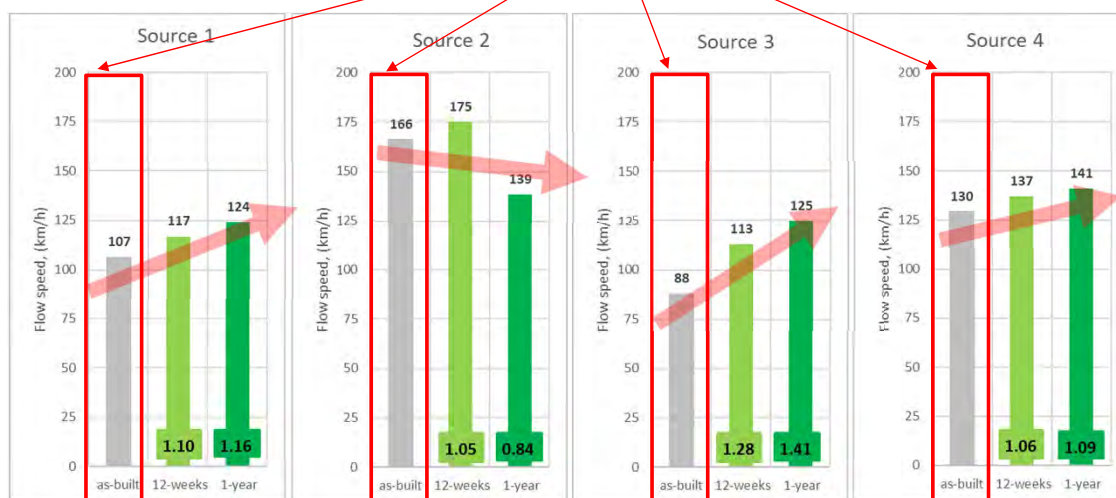
Effect of vegetation growth



Growth Modify Factor, **GMF**

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The standard can be based on the "As-built" performance and predict the 1 year performance



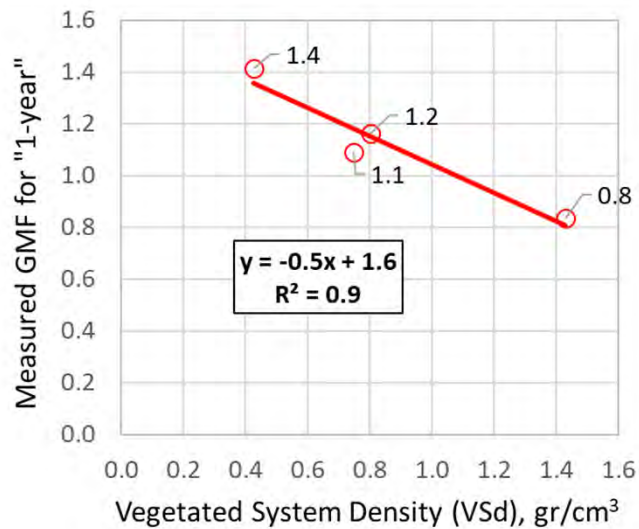
density "as-built" **0.80** g/cm³

1.43

0.43

0.75

50



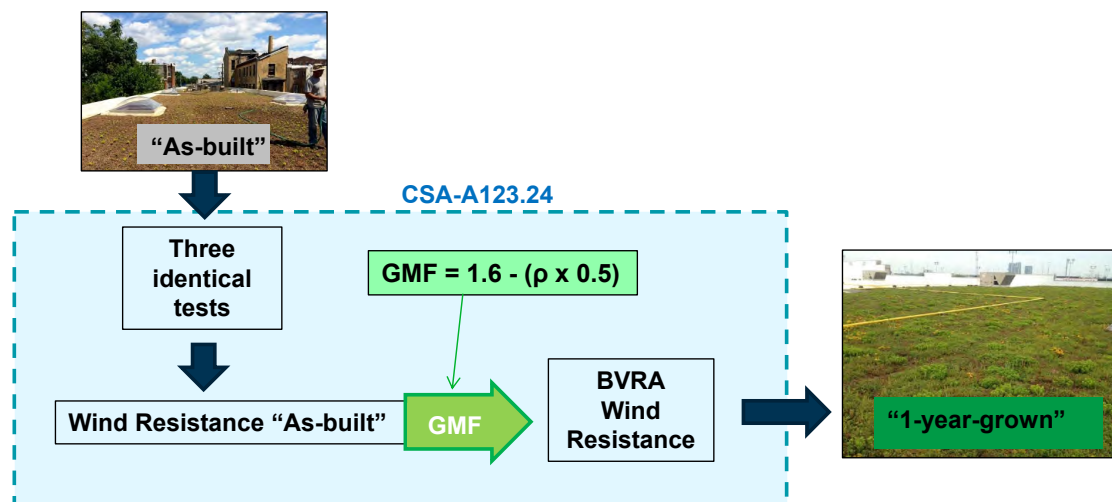
$$GMF = 1.6 - \frac{\rho}{2}$$

ρ (g/cm³), density "as-built"

(*) GMF no greater than 1.3

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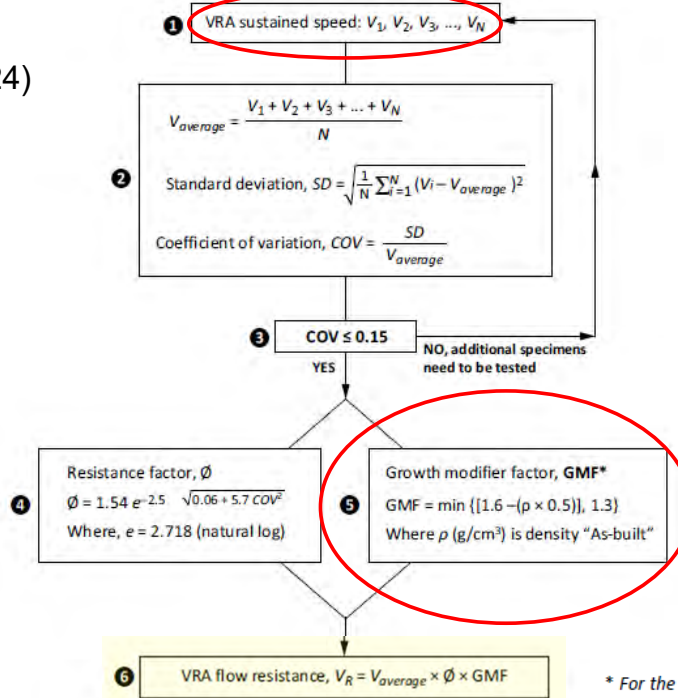
Standard approach



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Flow chart (from CSA123.24)

Tests "as-built"

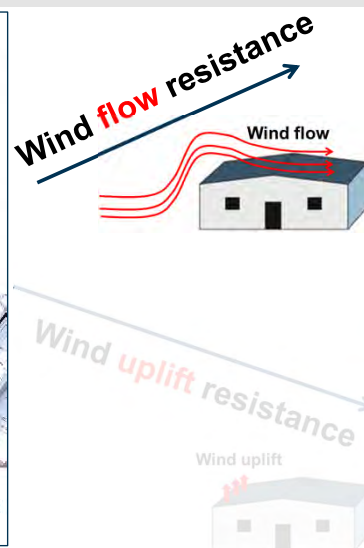


To account for the vegetation growth: **GMF**

Depends on "as-built" density

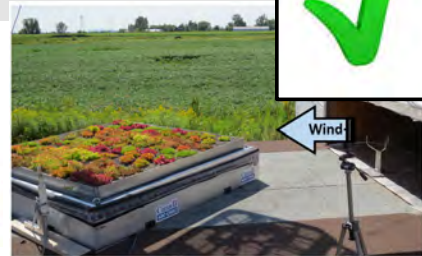
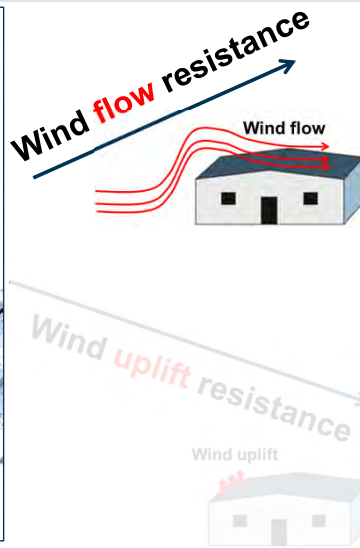
53

VRA wind resistance



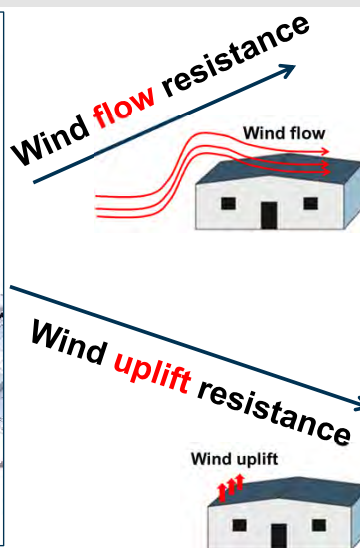
54

VRA wind resistance



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VRA wind resistance

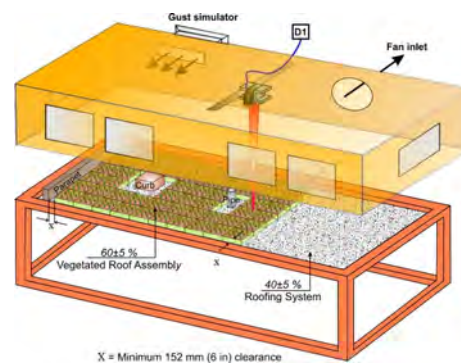
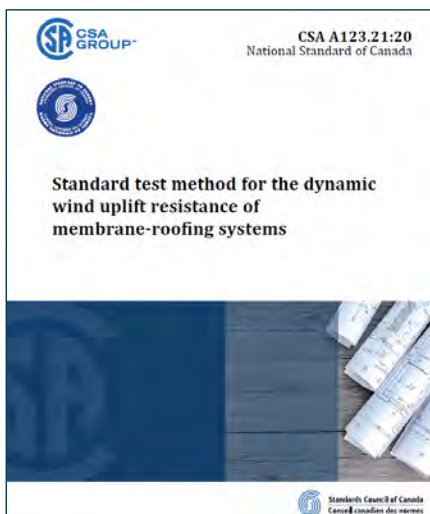


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Wind Uplift Resistance

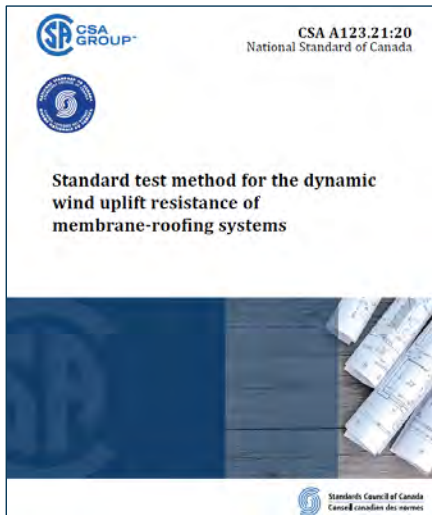
57

Wind uplift resistance



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Wind uplift resistance



MARS (Not applicable to VRA)

AARS

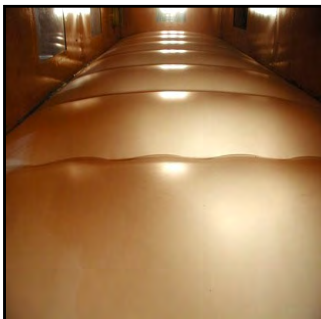


PARS

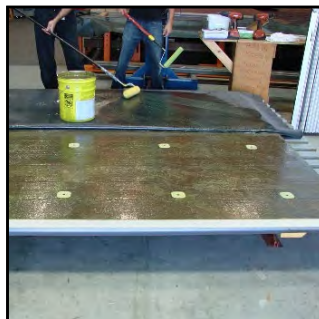


Wind uplift resistance

X
MARS



PARS



AARS



Wind uplift resistance

Roofing System Construction



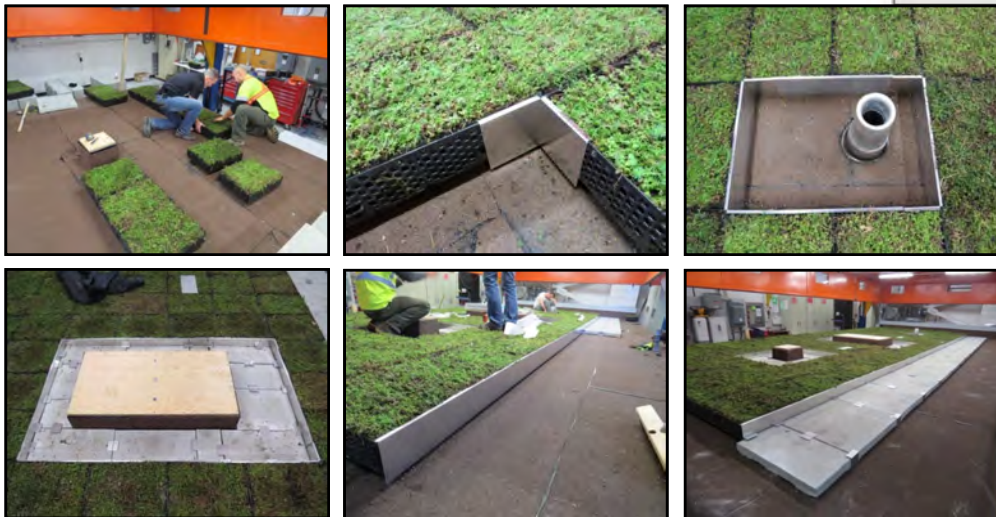
Wind uplift



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Wind uplift resistance

Example: MVRA System Construction



Wind uplift



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Typical uplift testing



Wind uplift



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Failure mode

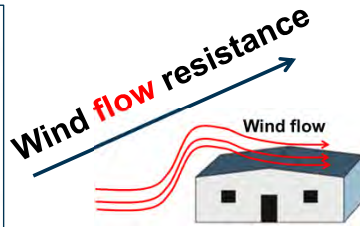


Wind uplift



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VRA wind resistance

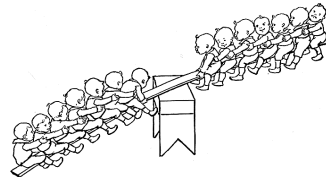


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Application

3 steps

- 1- Design wind data (pressure and wind speed) from **Code**
- 2- Resistance by testing using **CSA 123.24**
- 3- Code **VERIFICATION**:

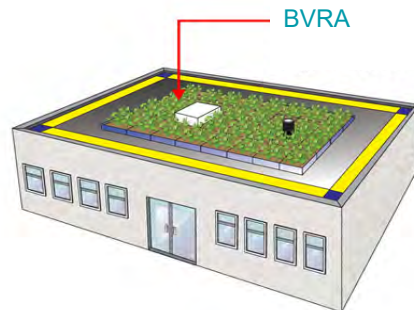


Resistance (P_r, V_r) > Design (P_d, V_d) ●●● 66

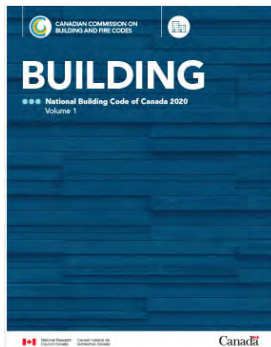
Application

A building-owner wants to install a **BVRA** on a building.

Two options of **BVRAs** (Source_1 and Source_2)



1- Design



Design
wind **uplift**

Design
wind **speed**

Part 4 Structural Design

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Table C-2
Climatic Design Data for Selected Locations in Canada

Province and Location	Elev. m	Design Temperature				Design Wind Speed km/h	15 min. Wind Speed km/h	Basic Snow Load kN/m²	Basic Ice Load kN/m²	Design Rainfall mm/day	Mean Sea Level Pressure, kPa		
		20% C	1% C	0.2% C	0.02% C						SL	IL	ISO
Atlantic Region													
Newfoundland	25	-24	-31	-35	-40	100	100	0.0	0.0	150	10.0	0.0	10.0
Quebec	30	-16	-23	-27	-32	100	100	0.0	0.0	150	10.0	0.0	10.0
Quebec City	30	-16	-23	-27	-32	100	100	0.0	0.0	150	10.0	0.0	10.0
Montreal	30	-16	-23	-27	-32	100	100	0.0	0.0	150	10.0	0.0	10.0
Ottawa	30	-16	-23	-27	-32	100	100	0.0	0.0	150	10.0	0.0	10.0
Halifax	30	-16	-23	-27	-32	100	100	0.0	0.0	150	10.0	0.0	10.0
St. John's	30	-16	-23	-27	-32	100	100	0.0	0.0	150	10.0	0.0	10.0
Thunder Bay	200	-24	-31	-35	-40	100	100	0.0	0.0	150	10.0	0.0	10.0
Windsor	180	-24	-31	-35	-40	100	100	0.0	0.0	150	10.0	0.0	10.0
Chicago	180	-24	-31	-35	-40	100	100	0.0	0.0	150	10.0	0.0	10.0
St. Louis	180	-24	-31	-35	-40	100	100	0.0	0.0	150	10.0	0.0	10.0
St. Paul	180	-24	-31	-35	-40	100	100	0.0	0.0	150	10.0	0.0	10.0
Minneapolis	180	-24	-31	-35	-40	100	100	0.0	0.0	150	10.0	0.0	10.0
Des Moines	180	-24	-31	-35	-40	100	100	0.0	0.0	150	10.0	0.0	10.0
Omaha	180	-24	-31	-35	-40	100	100	0.0	0.0	150	10.0	0.0	10.0
Lincoln	180	-24	-31	-35	-40	100	100	0.0	0.0	150	10.0	0.0	10.0
Indianapolis	180	-24	-31	-35	-40	100	100	0.0	0.0	150	10.0	0.0	10.0
Columbus	180	-24	-31	-35	-40	100	100	0.0	0.0	150	10.0	0.0	10.0
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Lincoln	180	-24	-31	-35	-40	100	100	0.0	0.0	150	10.0	0.0	10.0
Indianapolis	180	-24	-31	-35	-40	100	100	0.0	0.0	150	10.0	0.0	10.0
Columbus	180	-24	-31	-35	-40	100	100	0.0	0.0	150	10.0	0.0	10.0
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Indianapolis	180	-24	-31	-35	-40	100	100	0.0	0.0	150	10.0	0.0	10.0
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Dayton	180	-24	-31	-35	-40	100	100	0.0	0.0	150	10.0	0.0	10.0
Cincinnati	180	-24	-31	-35	-40	100	100	0.0	0.0	150	10.0	0.0	10.0
St. Louis	180	-24	-31	-35	-40	100	100	0.0	0.0	150	10.0	0.0	10.0
St. Paul	180	-24	-31	-35	-40	100	100	0.0	0.0	150	10.0	0.0	10.0
Minneapolis	180	-24	-31	-35	-40	100	100	0.0	0.0	150	10.0	0.0	10.0
Des Moines	180	-24	-31	-35	-40	100	100	0.0	0.0	150	10.0	0.0	10.0

1- Design



Design
wind **uplift**

Part 4 Structural Design

4.1. Structural Loads and Procedures	
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National Research Council Canada

<https://nrc.canada.ca/software-applications/wind-roo...>

Wind-Roof Calculators on the Internet (Wind-RCI)

Apr 5, 2023 — This web application determines wind loads for roof cladding and modular vegetated roof assembly design parameters based on the National ...

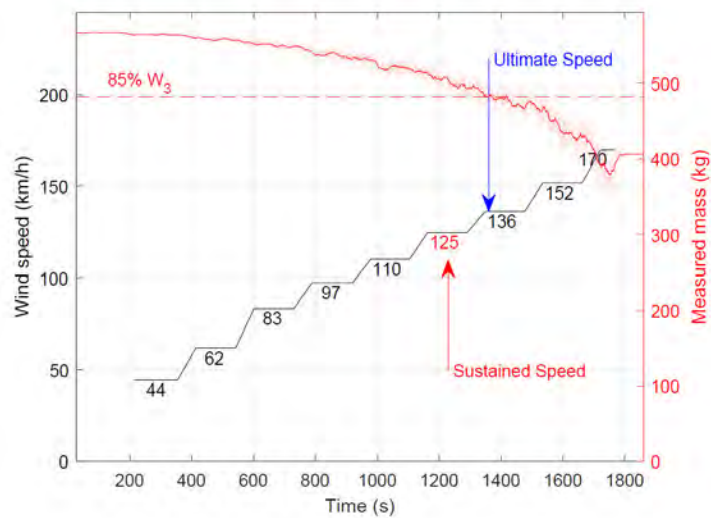
Parameters	25	30	35	40	45	50	55	60	65	70	75	80	85	90	95	100	105	110	115	120	125	130	135	140	145	150
Mean	25	30	35	40	45	50	55	60	65	70	75	80	85	90	95	100	105	110	115	120	125	130	135	140	145	150
Standard Deviation	10	12	14	16	18	20	22	24	26	28	30	32	34	36	38	40	42	44	46	48	50	52	54	56	58	60
Skewness	0.1	0.2	0.3	0.4	0.5	0.6	0.7	0.8	0.9	1.0	1.1	1.2	1.3	1.4	1.5	1.6	1.7	1.8	1.9	2.0	2.1	2.2	2.3	2.4	2.5	
Kurtosis	1.0	1.2	1.4	1.6	1.8	2.0	2.2	2.4	2.6	2.8	3.0	3.2	3.4	3.6	3.8	4.0	4.2	4.4	4.6	4.8	5.0	5.2	5.4	5.6	5.8	6.0

2- Resistance FLOW



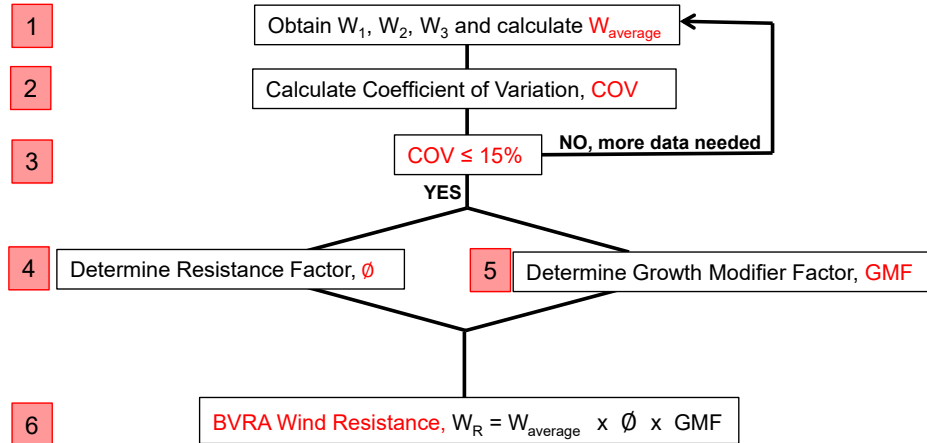
71

2- Resistance FLOW: typical result



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2- Resistance Wind Flow



Lab work!

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2- Resistance WIND SPEED

		Source_1	Source_2	
(i) Three identical tests (W_1, W_2, W_3)	$W_{average}$	112 km/h	148 km/h	1
(ii) Standard deviation,	SD	14.86	9.90	2
(iii) Coefficient of Variation, COV		11%	6%	3
Resistance factor,	ϕ	0.64	0.70	4
Average "as-built" density, ρ (g/cm ³)		0.80	1.00	
GMF = $1.6 - (\rho \times 0.5)$		1.20	1.10	5
$W_R = W_{average} \times \phi \times GMF$		86 km/h	114 km/h	6

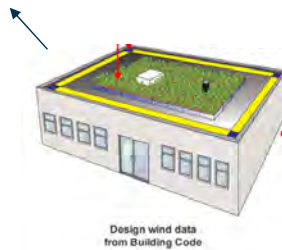
$COV \leq 15\%$ ✓

Lab results

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3- Verification

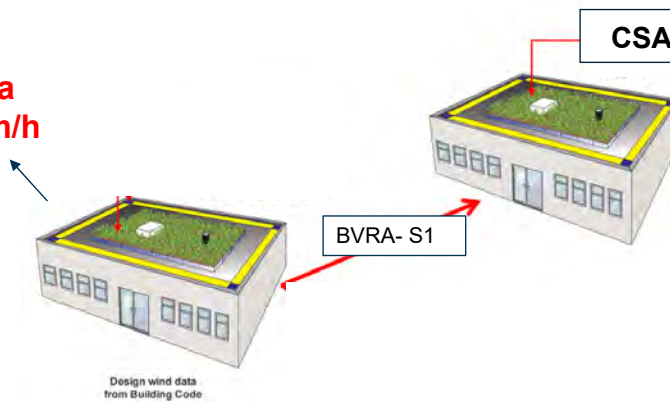
$P_d = -2.5\text{kPa}$
 $V_d = 108\text{ km/h}$



75

3- Verification

$P_d = -2.5\text{kPa}$
 $V_d = 108\text{ km/h}$

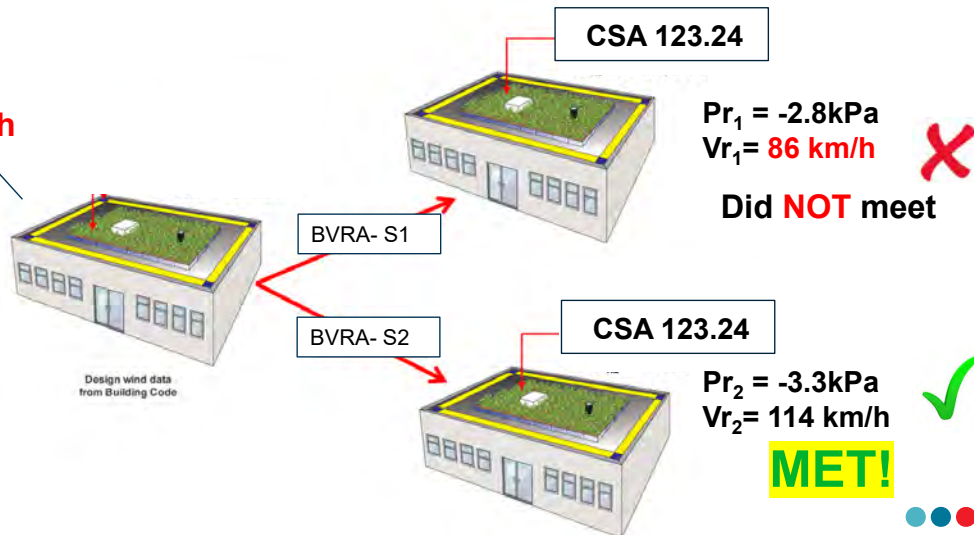


$P_{r1} = -2.8\text{kPa}$
 $V_{r1} = 86\text{ km/h}$ **X**
Did NOT meet

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3- Verification

$P_d = -2.5 \text{ kPa}$
 $V_d = 108 \text{ km/h}$



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Journal of Architectural Engineering / Volume 27 Issue 3 - September 2021



ASCE

New Test Methodology for Wind Resistance Evaluation of Built-In-Place Vegetated Roof Assembly

Appupillai Baskaran, M.ASCE¹; Mauricio Chavez²; and Sudhakar Molleti³

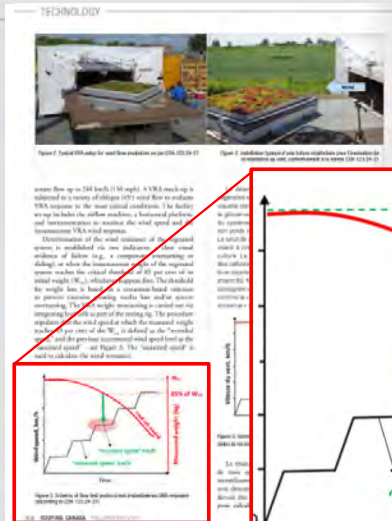
Abstract: The North American Vegetated Roof Assembly (VRA—a.k.a. green roofs) market is dominated by two different types: modular vegetated roof assemblies (MVRA) and built-in-place vegetated roof assemblies (BVRA). In MVRA, the vegetation is pregrown in transportable trays and installed on the roof, whereas in the BVRA, the vegetation develops on the roof. In 2015, the National Research Council of Canada (NRC), in collaboration with the green roof industry and roofing industry, set the national standard for the wind resistance evaluation of MVRA. Practitioners and building authorities have widely used this standard. In 2017, NRC and the industry collaborators started a new research project on BVRA to expand the current standards. The wind performance of BVRA is highly dependent on the growth stage of the vegetation. This variable was investigated by testing four BVRA sources (S1, S2, S3, and S4) at three different growth stages, namely, *as-built*, 12 weeks, and 1 year of growth. The interaction between the approaching wind speed and the BVRA response was monitored by installing load cells underneath the test mock-up. The load cells were intended to capture the growth media loss as the wind flow develops over the BVRA mock-up. The wind speed at which the vegetated system's (VS) weight reaches 85% of the initial weight was used to compute the BVRA wind performance. The tests conducted at the three growth stages permitted developing an empirical growth modifier factor (GMF). The GMF is a practical engineering solution to estimate the wind performance of a 1-year BVRA using the *as-built* performance data. The paper presents the development of this new testing methodology and the standardization process. DOI: 10.1061/(ASCE)AE.1943-5568.0000475. © 2021 American Society of Civil Engineers.

Author keywords: Built-in-place vegetated roof assemblies; Green roofs; Wind erosion; Wind resistance; Standard development; Building code.

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CRCA magazine fall/winter 2021



NBCC

Canadian Board for Harmonized Construction Codes

1754

Proposed Change 1754

Code Reference(s):	NBC20 Div.B 5.2.2.2. (first printing)
Subject:	Vegetated Roof Assemblies
Title:	Requirements for Wind Resistance of Vegetated Roof Assemblies
Description:	This proposed change introduces a requirement for the testing of the dynamic wind uplift resistance and wind flow resistance of vegetated roof assemblies in accordance with the CAN/CSA-A123.24:21 standard.
Related Code Change Request(s):	CCR 1151

NBCC

PROPOSED CHANGE

[5.2.2.2.] 5.2.2.2. Determination of Wind Load

[5] 5) Membrane roofing assemblies with proven past performance for the anticipated wind loads need not comply with Sentence (4). (See Note A-5.1.4.1.(5).)

[6] --) The wind resistance of vegetated roof assemblies shall

- a) --) conform to existing provincial or territorial regulations, or
- b) --) in the absence of the regulations referred to in Clause (a), be determined in accordance with the requirements of CAN/CSA-A123.24:21, "Standard test method for wind resistance of vegetated roof assembly" (see Note A-5.2.2.2.(6)(b)).

Note A-5.2.2.2.(6)(b) Vegetated Roof Assemblies.

When a vegetated system is added on the top of a membrane roofing assembly, a vegetated roof assembly (VRA) is formed. The test methods described in CAN/CSA-A123.24:21, "Standard test method for wind resistance of vegetated roof assembly," determine both the wind uplift resistance and the wind flow resistance of the VRA. If the wind uplift resistance of the membrane roofing assembly used in the VRA has already been determined in accordance with the requirements of CAN/CSA-A123.21, "Standard test method for the dynamic wind uplift resistance of membrane-roofing systems," as required by Sentence 5.2.2.2.(4), then this resistance can be used as an acceptable conservative wind uplift resistance of the VRA; in such cases, only the wind flow resistance of the VRA has to be determined in accordance with CAN/CSA-A123.24:21. If, however, any variations in the components or methods of construction of the membrane roofing assembly used in the VRA are made after the wind uplift resistance was determined in accordance with the requirements of CAN/CSA-A123.21, then the wind uplift resistance of the VRA must be determined in accordance with CAN/CSA-A123.24:21.

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Questions?

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